

## Profile functions used in Jana2020

The profile functions are used to model the shape of diffraction peaks. It is a function of the argument  $x = \theta - \theta_{\mathbf{h}}$ , the difference between the actual position and the expected position of the diffraction  $\mathbf{h}$ . There are three possible profile functions in Jana2020.

**Gaussian function:**  $G(x) = a_G \exp(-x^2 / 2b_G^2)$  (1)

The coefficients  $a_G$   $b_G$  can be expressed as a function of FWHM called  $H_G$  :

$$a_G = \frac{2}{H_G} \sqrt{\frac{\ln 2}{\pi}} \quad b_G^2 = \frac{H_G^2}{8 \ln 2} \quad (2)$$

**Lorentzian function:**  $L(x) = \frac{a_L}{1 + (2x/b_L)^2}$  y (3)

Similarly, as for the Gaussian, the coefficients  $a_L$  and  $b_L$  can be expressed as a function of  $H_L$  :

$$a_L = \frac{2}{\pi H_L} \quad b_L = H_L \quad (4)$$

**Pseudo-Voigt function:**  $pV(x) = \eta L(x) + (1 - \eta)G(x)$  (5)

Both FWHM for Lorentzian and Gaussian parts in the above formula are supposed to be the same, calculated from the equation:

$$H = H_G^5 + 2.69269 H_G^4 H_L + 2.42843 H_G^3 H_L^2 + 4.47163 H_G^2 H_L^3 + 0.07842 H_G H_L^4 + H_L^5 \quad (6)$$

The second parameter  $\eta$ :

$$\eta = 1.36603 \frac{H_L}{H} - 0.47719 \left( \frac{H_L}{H} \right)^2 + 0.11116 \left( \frac{H_L}{H} \right)^3 \quad (7)$$

### **Angular dependence of FWHM**

The FWHM parameters are dependent on the scattering angle. The Gaussian  $H_G$  is composed of five terms:

$$b_G^2 = U \tan^2 \theta + V \tan \theta + W + \frac{P}{\cos^2 \theta} + (1 - \zeta)^2 \Gamma_A^2 \quad (8)$$

The first three terms account for basic broadening due to slits, wavelength dispersion, and the monochromator, as described by Cagliotti, Pauletti & Ricci (1958, Nucl. Instrum., **3**,

223). The fourth term is the Scherrer coefficient for Gaussian broadening. It should be noted that only U and W or P and W or P and U can be refined together to avoid singularity caused by the trigonometric relationship  $\tan^2 \theta + 1 = \frac{1}{\cos^2 \theta}$ . The last term accounting for anisotropic strain will be discussed separately.

The Lorentzian  $b_L$  is composed of five terms as well:

$$b_L = (X + X_e \cos \phi_X) / \cos \theta + (Y + Y_e \cos \phi_Y) \tan \theta + \zeta \Gamma_A \quad (9)$$

The  $X$  terms account for Lorentzian Scherrer particle broadening.  $X$  and  $X_e$  stands for isotropic and anisotropic parts, respectively.  $\phi_X$  is the angle between the diffraction vector and the broadening direction.

The  $Y$  terms describe strain broadening, and the meaning of the constants is analogous to that for particle broadening.

The last term represents Stephens's strain anisotropy and cannot be combined with  $Y_e$ .

### Anisotropic peak broadening as introduced by P.W.Stephens

The phenomenological model is based on a general tensor expression in which a symmetrical 4th order tensor describes the anisotropic strain:

$$\sigma^2(hkl) = D^{ijmn} h_i h_j h_m h_n = \sum_{HKL} S_{HKL} h^H k^K l^L$$

The first term is a general tensor expression using the Landau summation convention, allowing a simple derivation of symmetry restrictions similar to those for 4th-order ADP parameters. The second term has the explicit form used by Stephens, in which the summation is restricted to  $H + K + L = 4$ .

Using the Bragg equation, we can finally get the contribution to FWHM :

$$\Gamma_A = \left[ \sigma^2(h, k, l) \right]^{1/2} d^2 \tan \theta$$

The ratio of the broadening between the Gaussian and Lorentzian parts is  $(1 - \zeta) / \zeta$ .

Jana2000 uses the notation similar to that in GSAS:

$$U \rightarrow GU, V \rightarrow GV, W \rightarrow GW, P \rightarrow GP$$

$$X, X_e \rightarrow LX, LX_e, Y, Y_e \rightarrow LY, LY_e$$

The Stephens' parameters are chosen in analogy to his paper - *J. Appl. Cryst.* (1999), **32**, 281-289.

### Origin shift parameters

shift – defines the zero shift (units of 0.01 deg).

sycos –in analogy with the Fullprof:  $\Delta 2\theta = c \cdot \cos \theta$  relates to a specimen displacement

sysin – in analogy with the Fullprof:  $\Delta 2\theta = s \cdot \sin 2\theta$  relates to a transparency correction

These three values are added to the theoretical peak position to obtain a position in the experimental profile.

### Different R values used in Jana2020

profile R-factor 
$$R_p = \frac{\sum_i |y_i(obs) - y_i(calc)|}{\sum_i y_i(obs)} \cdot 100$$

$i$  run over all points of the profile,  $y_i(obs)$  and  $y_i(calc)$  are the observed and calculated intensity, respectively.

weighted profile R-factor 
$$R_{wp} = \sqrt{\frac{\sum_i w_i (y_i(obs) - y_i(calc))^2}{\sum_i w_i y_i(obs)^2}} \cdot 100$$

where the weights are calculated from standard uncertainties of profile intensities:

$$w_i = \frac{1}{\sigma^2 [y_i(obs)]}$$

experimental R factor 
$$R_{exp} = \sqrt{\frac{\sum_i w_i y_i(obs)^2}{n - p}} \cdot 100$$

$n$  number of profile points,  $p$  number of refined parameters

goodness of fit 
$$GOF = \frac{R_{wp}}{R_{exp}}$$

pure profile R-factor 
$$cR_p = \frac{\sum_i |y'_i(obs) - y'_i(calc)|}{\sum_i y'_i(obs)} \cdot 100$$

weighted profile R-factor 
$$cR_p = \frac{\sum_i w_i (y'_i(obs) - y'_i(calc))^2}{\sum_i w_i y'_i(obs)^2} \cdot 100$$

where  $y'_i(obs) = y_i(obs) - b_i$  and  $y'_i(calc) = y_i(calc) - b_i$  are intensities corrected for background.

The conventional structural R values are calculated after the le Bail separation. The R values based on F and I are listed for both all and observed reflections. The R factor based on F is  $R_F(obs)$ ,  $R_F w(obs)$ ,  $R_F(all)$ ,  $R_F w(all)$ . Those based on intensities are  $R_B(obs)$ ,  $R_B w(obs)$ ,  $R_B(all)$ ,  $R_B w(all)$ .

### **Extraction of $F_{obs}$ and $\sigma(F_{obs})$ from powder profile**

Powder diffraction: the  $F_{hkl}(obs)$  values for the calculation of Fourier maps, structural R values, and MEM are to be derived from the observed and calculated powder profiles and  $F_{hkl}(calc)$  as follows from the temporary structural model. From all profile points to which the reflection  $(h, k, l)$  contributes, we can write:

$$L_i \cdot A_i \cdot R_i \cdot P_i(h, k, l) \Omega_i(h, k, l) F_{hkl}^2(obs) = \frac{y'_i(obs)}{y'_i(calc)} \cdot L_i \cdot A_i \cdot R_i \cdot P_i(h, k, l) \Omega_i(h, k, l) F_{hkl}^2(calc)$$

$L_i$  contains the Lorentz, polarization, and multiplicity factor of the reflection  $(h, k, l)$

$A_i$  is an absorption factor

$R_i$  is a roughness correction

$P_i(h, k, l)$  is the preference orientation function

$\Omega_i(h, k, l)$  is the reflection profile function

It means that for all profile points to which the reflection  $(h, k, l)$  makes a non-zero contribution, we have  $F_{hkl,i}^2(obs)$ :

$$F_{hkl,i}^2(obs) = \frac{y'_i(obs)}{y'_i(calc)} \cdot F_{hkl}^2(calc)$$

Then the final values  $F_{hkl}^2(obs)$  and  $\sigma[F_{hkl}^2(obs)]$  can be calculated as an average and standard error.

However, as profile points do not have the same experimental accuracy, two methods to suppress undesired fluctuations:

1. For the calculation of averaged values, only profile points to which the relevant reflection  $(h, k, l)$  contributes significantly are used. As a criterion, we are using values of the profile function  $\Omega_i(h, k, l)$  which must be at least 10% of its maximal value.

2. In the average procedure, we use weights based on experimental standard uncertainties:

$$F_{hkl}^2(obs) = \frac{\sum_i w_i \frac{y'_i(obs)}{y'_i(calc)} F_{hkl}^2(calc)}{\sum_i w_i}$$

The weights  $w_i$  are derived from the estimated values of standard uncertainties of the expression:

$$Y_i = \frac{y'_i(obs)}{y'_i(calc)} = \frac{y_i(obs) - b_i}{y_i(calc) - b_i}$$

Following the propagation rule, we have:

$$\sigma^2(Y_i) = 1/w_i = \left[ \frac{-1}{y_i(calc) - b_i} \right]^2 \sigma^2[y_i(obs)] + \left[ \frac{(y_i(obs) - b_i)}{(y_i(calc) - b_i)^2} \right]^2 \sigma^2[y_i(calc)] + \left[ \frac{-y_i(calc) + y_i(obs)}{(y_i(calc) - b_i)^2} \right]^2 \sigma^2[b_i]$$

The values  $\sigma[y_i(calc)]$  and  $\sigma[b_i]$  are estimated from experimental  $\sigma[y_i(obs)]$ :

$$\sigma[y_i(calc)] = \frac{y_i(calc)}{y_i(obs)} \sigma[y_i(obs)] \quad \sigma[b_i] = \frac{b_i}{y_i(obs)} \sigma[y_i(obs)]$$

Then for  $\sigma^2(Y)$  we have:

$$1/w_i = \sigma^2[y_i(obs)] \left[ \frac{1}{(y_i(calc) - b_i)^2} + \left\{ \frac{y_i(obs) - b_i}{(y_i(calc) - b_i)^2} \frac{y_i(calc)}{y_i(obs)} \right\}^2 + \left\{ \frac{y_i(obs) - y_i(calc)}{(y_i(calc) - b_i)^2} \frac{b_i}{y_i(obs)} \right\}^2 \right]$$

A similar method is used for the estimation of  $\sigma[F_{hkl}^2(obs)]$ :

$$\sigma[F_{hkl}^2(obs)] = \sqrt{\frac{\sum_i w_i \left[ \frac{y'_i(obs)}{y'_i(calc)} F_{hkl}^2(calc) \right]^2}{\sum_i w_i} - F_{hkl}^4(obs)}$$

This method combines experimental standard uncertainties expressed by weights with a profile fit. In the case that peaks are too sharp, it could be preferable to concentrate only on experimental uncertainties and calculate  $\sigma[F_{hkl}^2(obs)]$  using the error propagation formula:

$$\sigma[F_{hkl}^2(obs)] = \frac{\sqrt{\sum_i w_i F_{hkl}^4(calc)}}{\sum_i w_i}$$

This equation follows from the expression for  $F_{hkl}^2(obs)$ :

$$F_{hkl}^2(obs) = \frac{\sum_i w_i \frac{y_i'(obs)}{y_i'(calc)} F_{hkl}^2(calc)}{\sum_i w_i}$$

and the application of the error propagation theorem under the assumption that the terms in the summation have zero correlations:

$$\sigma[F_{hkl}^2(obs)] = \sqrt{\frac{1}{\left(\sum_i w_i\right)^2} \left(\sum_i w_i^2 \sigma^2(Y_i) F_{hkl}^4(calc)\right)} = \frac{\sqrt{\sum_i w_i F_{hkl}^4(calc)}}{\sum_i w_i}$$

### **Particle size and strain parameters as follows from the Jana profile parameters**

The particle size and strain parameter are usually expressed as functions of the integral breadth  $\beta$ , which represents the width of a rectangle with the same height and area as the diffraction peak.

#### **Gaussian distribution:**

$$G(x) = a_G \exp(-x^2 / 2b_G^2)$$

$$\Rightarrow \beta_G = \frac{H_G}{2} \sqrt{\frac{\pi}{\ln 2}} = \sqrt{2\pi} b_G$$

$$a_G = \frac{2}{H_G} \sqrt{\frac{\ln 2}{\pi}} \quad b_G^2 = \frac{H_G^2}{8 \ln 2}$$

#### **Lorentzian distribution:**

$$L(x) = \frac{a_L}{1 + (2x/b_L)^2}$$

$$\Rightarrow \beta_L = \frac{\pi H_L}{2} = \frac{\pi b_L}{2}$$

$$a_L = \frac{2}{\pi H_L} \quad b_L = H_L$$

The particle size is generally associated with the line broadening proportional to  $\frac{1}{\cos \theta}$ . It means that, for the Gaussian distribution, it is related to the parameter P (equation (8)), and for the Lorentzian distribution, to the parameter X (equation (9)).

According to the Scherrer formula for  $D_V$  the so-called volume weighted crystalline size, we have:

$$D_V = K\lambda/(\beta \cos \theta)$$

K = Scherrer constant, a somewhat arbitrary value that falls in the range 0.87-1.0. I usually assume K = 1.

$\lambda$  = wavelength of the radiation

$\beta$  = integral breadth of a reflection (in radians) located at  $2\theta$ .

For the Gaussian distribution, we have from equations (8):

$$D_V = 180 K\lambda/(\sqrt{2\pi^3 P}) \quad \text{if P expressed in degs}^2 \text{ (Fullprof) or}$$

$$D_V = 18000 K\lambda/(\sqrt{2\pi^3 P}) \quad \text{if P expressed in (0.01 degrees)}^2 \text{ (GSAS, Jana)}$$

For the Lorentzian distribution, we have from equation (9):

$$D_V = 360 K\lambda/(\pi^2 X) \quad \text{if X is expressed in degrees (Fullprof) or}$$

$$D_V = 36000 K\lambda/(\pi^2 X) \quad \text{if X is expressed in 0.01 degrees (GSAS, Jana)}$$

The strain parameter is generally associated with the line broadening proportional to  $\tan \theta$

$$\beta = 4\varepsilon_{str} \tan \theta$$

Where  $\beta$  are expressed in radians. For the Gaussian distribution, we have from equations (8):

$$\varepsilon_{str,G} = \sqrt{2\pi^3 U}/720 \quad \text{if U expressed in degrees}^2 \text{ (Fullprof) or}$$

$$\varepsilon_{str,G} = \sqrt{2\pi^3 U}/72000 \quad \text{if U expressed in (0.01degrees)}^2 \text{ (GSAS, Jana)}$$

For the Lorentzian distribution, we have from equations (9):

$$\varepsilon_{str,L} = \pi^2 Y/1440 \quad \text{if Y is expressed in degrees (Fullprof) or}$$

$$\varepsilon_{str,L} = \pi^2 Y/144000 \quad \text{if Y is expressed in 0.01degrees (GSAS, Jana)}$$

**However, such an interpretation has real meaning only if we are correcting the integral breadth for instrumental broadening.**

An alternative, more elegant approach is a fundamental one. In the Jana2020 program, we have used the approach developed by A.Coelho and R.W.Cheary:

*J. Appl. Cryst.* (1992). **25**, 109-121.

*J. Appl. Cryst.* (1998). **31**, 851-861.

*J. Appl. Cryst.* (1998). **31**, 862-868.

Particle size:

Instead of parameters X in equation (9), the so-called apparent crystallite size is used:

$$T_{app} = 18000 \lambda / (\pi X)$$

in Jana2020, this parameter is expressed in nm, and its relationship to  $D_V$  is:

$$D_V = (2K/\pi) T_{app}$$

For the Gaussian distribution, we are using the reduced form of equation (8):

$$b_G^2 = U \tan^2 \theta + \frac{P}{\cos^2 \theta} + (1 - \zeta)^2 \Gamma_A^2$$

where instead of the parameter P, we also use the apparent crystallite size:

$$T_{app} = \sqrt{8 \ln 2} 18000 \lambda / (\pi \sqrt{P}) \Rightarrow D_V = K \sqrt{\frac{4 \ln 2}{\pi}} T_{app}$$

The strain parameters  $U_{FA}$  and  $Y_{FA}$  (in Jana2020 called StrainG and StrainL) are just transformed to radians/100.

$$Y_{FA} = \pi Y / 180$$

$$U_{FA} = \pi \sqrt{8 \ln 2} U / 180$$

The factor  $\sqrt{8 \ln 2}$  transforms  $b_G$  to  $H_G$  according to the equation (2).

Then the parameter  $\varepsilon_{str,L}$  and  $\varepsilon_{str,G}$  are related to  $Y_{FA}$  and  $U_{FA}$ :

$$\varepsilon_{str,L} = \pi Y_{FA} / 800$$

$$\varepsilon_{str,G} = \sqrt{\frac{\pi}{4 \ln 2}} U_{FA} / 400$$